2D polynomial approach to stability of platoons of vehicles {Zdenek.Hurak, Michael.Sebek}@fel.cvut.cz



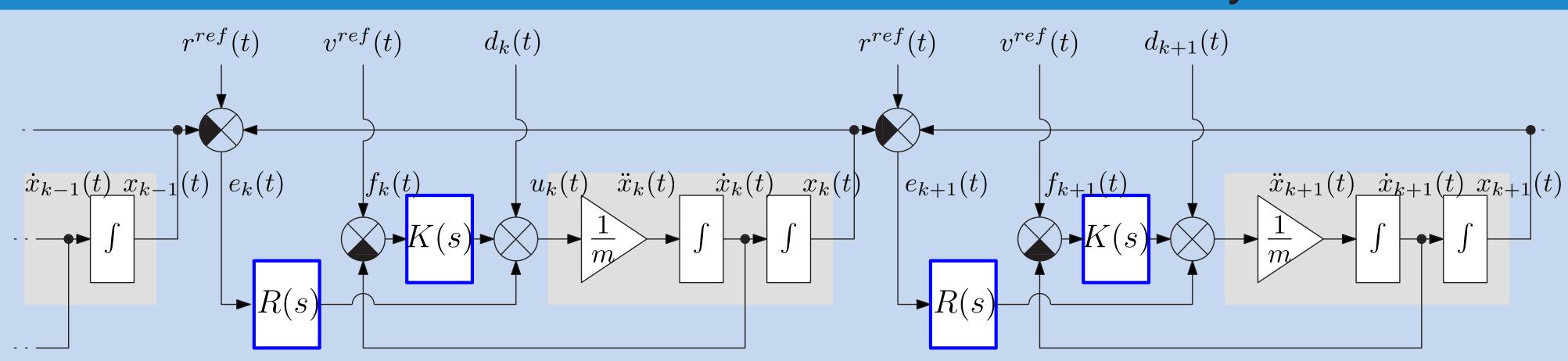
Contribution

We formulate the problem of stability testing and stabilization of an infinite platoon of vehicles within the 2D polynomial framework, that is, the dynamics of the problem is described using a fraction of two bivariate polynomials.

 $G(s,z) = \frac{b(s,z)}{a(s,z)}$

Analysing the two-variate denominator polynomial a(s, z) we can make conclusions about stability of a given feedback control configurations. For feedback configurations that admit a stabilizing solution, recent computational tools for positive polynomials can be used for stabilization.

Relative distance to the vehicle ahead and self-velocity available



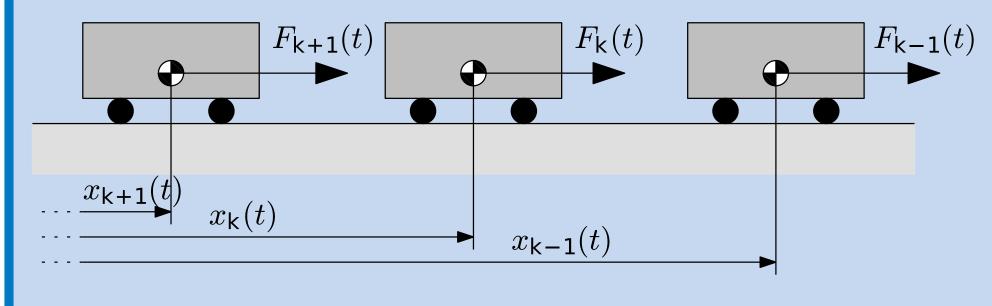
With the distance to the vehicle ahead measured which yields the closed-loop polynomial only, the transfer function is

 $\mathcal{O}(a, a)$

$$c(s, z) = ms^{2} + Ks + R(z^{-1} - 1)$$

Model

(Doubly) infinite platoon of vehicles indexed with $k = \{..., -1, 0, 1, 2, ...\}$. The dynamics of each vehicle is described by a simple double integrator. Positions denoted as $x_k(t)$ and velocities as $v_k(t)$.



Bilateral *z***-transform** is used in combination with Laplace tranform to get a transfer function relating the force $F_k(t)$ and distance to the vehicle ahead and self-velocity.

$$G(s,z) = -\frac{ms^2}{ms^2}$$

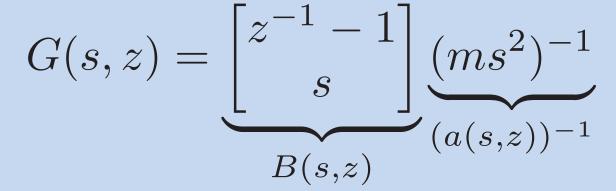
and the proportional controller is

C(s,z) = R

which makes the closed-loop polynomial

 $|c(s,z) = ms^2 + R(z^{-1} - 1)|$

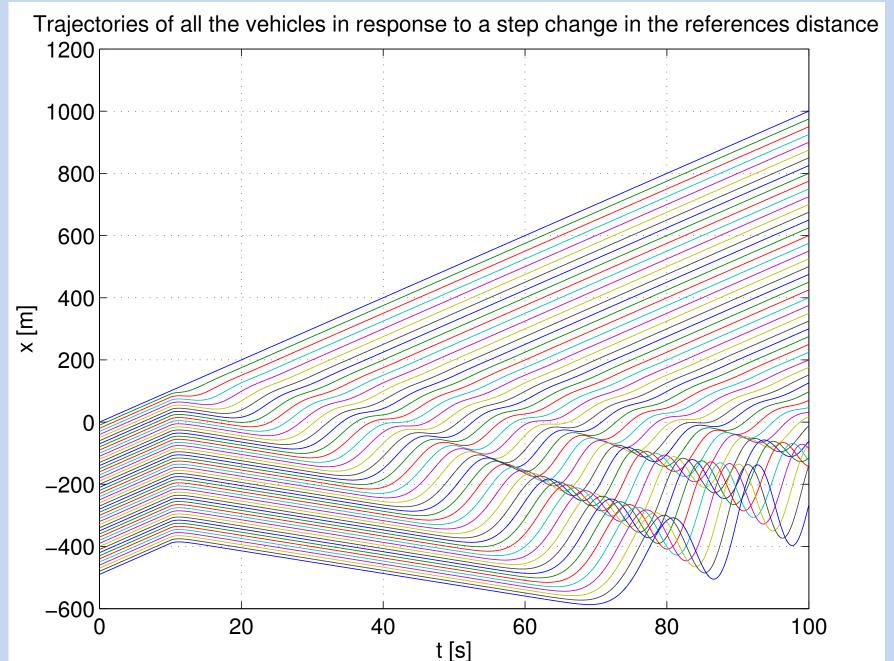
With the measurement of the absolute velocity



and proportional 2-input controller is

 $C(s,z) = \begin{bmatrix} R & K \end{bmatrix}$





No way to make the closed-loop characteristic polynomial stable by R and K (setting K low will achieve boundary of instability).

Absolute position available

2D polynomial stability

Spatially distributed system described by the transfer function $G(s, z) = \frac{b(s, z)}{a(s, z)}$ with the two polynomials free of a common factor is BIBO stable if $a(s, z) \neq 0$ for all s and z such that |z| = 1 and $\Re(s) \ge 0$. Apply this test to the closed-loop characteristic polynomial

c(s,z) = a(s,z)p(s,z) + b(s,z)q(s,z)

Open Questions

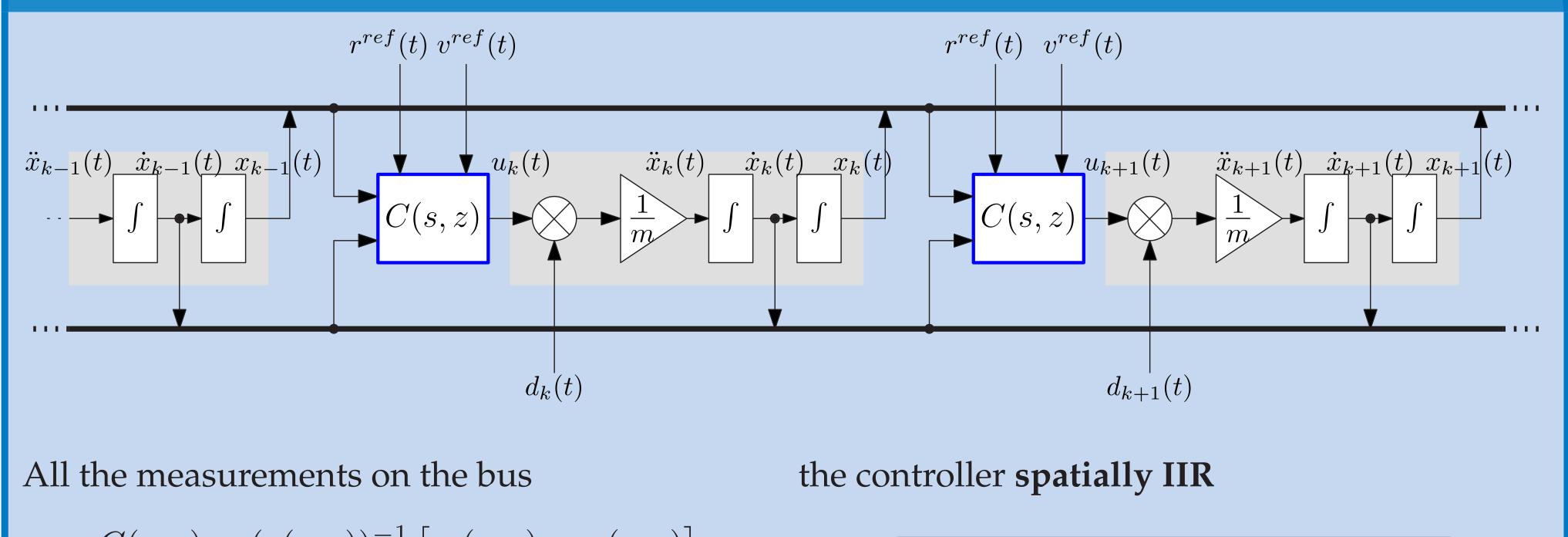
The use of the bilateral *z*-tranform assumes a doubly infinite string of vehicles. The **absence** of a leading vehicle may be misleading. Modifying the results for use with a unilateral *z*transform is the subject of our current research.

$$G(s,z) = \begin{bmatrix} z^{-1} - 1 \\ s \\ 1 \end{bmatrix} \frac{1}{ms^2}$$
$$C(s,z) = \begin{bmatrix} R & K & P \end{bmatrix}$$

$$c(s, z) = ms^{2} + Ks + R(z^{-1} - 1 + P)$$

Closed-loop stability can be achieved.

Global information available



Some references

- [Jovanović and Bamieh(2005)] On the ill-posedness of certain vehicular platoon control problems. Automatic *Control, IEEE Transactions on*, 50(9), 1307–1321.
- [Levine and Athans(1966)] On the optimal error regulation of a string of moving vehicles. Automatic Control, *IEEE Transactions on*, 11(3), 355–361.
- [Melzer and Kuo(1971)] Optimal regulation of systems described by a countably infinite number of objects. Automatica, 7(3), 359–366.
- [Peppard(1974)] String stability of relative-motion PID vehicle control systems. Automatic Control, IEEE Transactions on, 19(5), 579–581.
- [Seiler et al.(2004)] Disturbance propagation in vehicle strings. Automatic Control, IEEE Transactions on, 49(10), 1835–1842.

 $C(s,z) = (p(s,z))^{-1} [q_r(s,z) \quad q_v(s,z)]$ Q(s,z)

and the closed-loop polynomial is

c(s,z) = p(s,z)a(s,z) + Q(s,z)B(s,z)

For a particular choice

$$p = (z^{-1} - 1), q_r = R, q_v = K(z^{-1} - 1)$$

 $u_k(t) = u_{k-1}(t) + Rr_k(t) + Kv_k(t)$

and the closed-loop polynomial is

 $c(s,z) = (z^{-1}-1)ms^2 + R(z^{-1}-1) + K(z^{-1}-1)s$

 $= p(s,z)ms^2 + q_r(s,z)(z^{-1}-1) + q_v(s,z)s$ But $(z^{-1}-1)$ is not cancelled in all the closedloop transfer functions $(r_{ref} \rightarrow u)$. Nonessential singularity of the second kind appears. No way to BIBO stabilize with relative measurements?

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